Attorney Reference Number 23-65037-09 LMC:elv 08/31/09 E-1861 PCT US Application Number 10/581,281

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IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

in re application of: Larry C. Oisen et al.

PATENT

Application No. 10/581,281

Filed: May 31, 2006 Confirmation No. 3124

For: THERMOELECTRIC DEVICES AND APPLICATIONS FOR THE SAME.

Exeminer: Shannon M Gardner

Art Unit: 1795

Attorney Reference No. 23-65037-09

FILED VIA ELECTRONIC FILING SYSTEM COMMISSIONER FOR PATENTS.

DECLARATION UNDER 37 C.F.R. § 1,131

We, Larry C. Oisen, John G. DeSteese, Peter M. Martin, John W. Johnston and Timothy J. Peters, declare as follows:

- 1. We are joint inventors of the above-identified application,
- 2. We have reviewed the Office action dated April 30, 2009. It is our understanding that certain claims are rejected in the Office action dated April 30, 2009, as allegedly being anticipated under 35 U.S.C. § 102(e) by U.S. Pat. Pub. No. 2004/0231714 A1 ("Stark"), which has an alleged priority date of May 19, 2003. It is also our understanding that certain claims are rejected as allegedly being anticipated under 35 U.S.C. § 102(e) by U.S. Pat. Pub. No. 2004/0094192 ("Luo"), which has an alleged priority date of March 24, 2003.
 - 3. EVIDENCE OF REDUCTION TO PRACTICE AND OPERABILITY
 - Exhibit A hereto is a true copy of an Invention Report document signed prior to March 24. 2003, disclosing and illustrating reduction to practice inventions recited in certain of the pending claims.
 - > Exhibits B-1 and B-2 are computer screen shots showing photographs taken by Timothy Peters (and photographs alone) of equipment we had built and used to test and evaluate, prior to March 24, 2003, the embodiment of the power source of the invention that is shown in the photographs and as recited in certain of the pending claims.

Page 1 of 5

- Exhibit C is a computer screen shot showing a photograph taken prior to March 24, 2003 of an embodiment of the power source of the invention and as recited in certain of the pending claims, the power source embodiment being a flexible substrate with bismuth-telluride thermocouples and metal bridges between thermoelements, which embodiment we had built and tested prior to March 24, 2003.
- Exhibit D is a true copy of an Invention Report document signed prior to March 24, 2003, disclosing and likestrating conception of the invention as recited in certain of the pending claims.
- Exhibit E is a true copy of a PowerPoint document evidencing the reduction to practice and operability for its intended purpose, pnor to March 24, 2003, of an embodiment as recited in certain claims of this application, of an ambient thermal energy thermoelectric power source prototype (utilizing a commercially available thermoelectric module). Exhibit E including, e.g., page 1 being a graphical image of an embodiment of the ambient thermal energy thermoelectric power source prototype, page 2 showing an embodiment of circuitry of the thermoelectric power source prototype using a commercially obtained theremoelectric module (TE module) including a voltage amplifier with which the TE module operated, prior to March 24, 2003, to power an RF Tag, page 3 being a graph of the output of the TE power source prototype using ambient solar energy, prior to March 24, 2003, page 4 illustrating the contrast between a conventional discrete element TE module and a graphical illustration of an embodiment of the thin film TE module prototype (see Exhibit F for this prototype thin film TE module) used, prior to March 24, 2003, and page 5 being a photograph taken prior to March 24, 2003, showing a mock-up of the TE power source prototype using ambient thermal energy with the thin film TE module (see Exhibit F).
- Exhibit F is a true copy of a PowerPoint document evidencing reduction to practice and operability for its intended purpose, prior to March 24, 2003, of an embodiment as recited in certain claims of this application, of a thin film, thermoelectric power source device. Exhibit F includes, e.g., pages 1-4 with illustrations and photographs of bismuth telluride thin films used, prior to March 24, 2003, in prototypes of embodiments of the TE power source and of TE modules with such thin films, as recited in certain claims of the application, and page 5 showing thermographic imagery of a prototype thin film TE power source in operation, prior to March 24, 2003, with a temperature difference of about 6°C.
- Exhibit G are true copies of graphed data obtained from operation, prior to March 24, 2003, of a prototype of an embodiment of the TE power source having heat pipes, as recited in certain claims of the application, illustrating the operability of the TE power source for its intended purpose. For example, page 8 is a graph of the power responsive

Page 2 of 5

- to the temperature difference across a prototype thin film TE power source (with heat pipes) over the range 3°C to 22°C as measured prior to March 24, 2003
- Exhibit H is a true copy of tabulated data obtained, prior to March 24, 2003, from operation of a prototype of an embodiment of the TE power source having heat pipes, as recited in certain claims of the application, illustrating the operability of the TE power source for its intended purpose.

The redacted portions of the Exhibits do not qualify or dispute any of the unredacted portions.

- 4. We conceived of and reduced to practice in the United States apparatus and methods for generating electrical energy from an environment having two different temperature regions wherein we conceived and reduced to practice a thermoelectric power source (TE device) having a first side in communication with means for transmitting ambient thermal energy collected in a first temperature region using metallic wire thermocouples or thin him semiconductors assembled in alternating p- and n-type arrays, as recited in certain of the claims prior to March 24, 2003. See Exhibits A-H. For example, see Exhibit E, page 3 with a graph of the output of a commercially obtained TE module used in an embodiment of the TE power source as recited in certain of the claims for production of electrical energy using the TE module in the TE power source prototype using ambient solar energy, prior to March 24, 2003, and Exhibit F pages 1-3 illustrating an embodiment of the thin film theremocouples used in a TE power source prototype as recited in certain claims, prior to March 24, 2003, and page 4 being a prototype of the ambient thermal energy thin tilm TE power source and Exhibit F at page 5 showing thermographic imagery of the operation, prior to March 24, 2003, of a prototype of the thin film TE power source at a temperature difference of about 6°C.
- 5. We conceived of and reduced to practice in the United States of thermoelectric power source methods and apparatus as set forth in Item 4, having a second means for transmitting ambient energy collected in the second region by conduction, as recited in certain of the claims prior to March 24, 2003. See Exhibits A-H, for example, see Exhibit E, page 3 with a graph of the output of a prototype of the TE power source operating on ambient solar energy, prior to March 24, 2003, as recited in certain of the claims, page 5 a photograph taken prior to March 24, 2003, showing a prototype of an ambient thermal energy TE power source and Exhibit F at page 5 showing thermographic imagery of the operation, prior to March 24, 2003, of a prototype thin film TE device operating with a temperature difference of about 6°C, and the Exhibit H tabulation of data obtained from operation, prior to March 24, 2003, of a TE device having two neat pipes on a hot and a cold side, respectively. Heat is conducted to and from TE elements through the hot and cold shoes, respectively, the heat pipes, thereby transferring heat by convection, evaporation and condensation inside the heat pipes.

Page 3 of 5

- 6. We conceived of and reduced to practice in the United States the use of apparatus and methods as set forth in item 4 above having first and second temperature regions with differences of less than, equal to, or greater than 15°C, as recited in certain of the claims prior to March 24, 2003. See Exhibits A-H, for example, see Exhibit F at page 5 showing thermographic imagery of the operation, prior to March 24, 2003, of a prototype of the thin film TE device operating with a temperature difference of about 6°C.
- 7. We conceived of and reduced to practice in the United States a power source comprising the methods and apparatus as set forth in item 4 above, including a super capacitor and/or at least one voltage amplifier, as recited in certain claims, prior to March 24, 2003. See Exhibits A H. For example, Exhibit E, page 2 evidences the reduction to practice and operability for its intended purpose, prior to March 24, 2003 of a TE power source prototype capable of producing useful power by heating a hot shoe of the TE power source with solar energy while the cold side of the TE power source was transferring heat into the ground. The TE power source included a voltage amplifier to supply an energy storage means (super capacitor) to power an RF Tag that transmitted temperature data wirelessly to a nearby building.
- 8. All statements made herein and of our own knowledge are true and all statements made on information are believed to be true; and further, these statements were made with the knowledge that willful false statements and like are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code, and that any such willful false statements made may jeopardize the validity of the application or any patent issuing thereon.

LMC:ejv 08/91/09 E-1861 PCT US PATENT Attorney Reference Number 23-65037-09 Application Number 10/581,281

Date 09/09/2009

John W. Johnston

Date 69/16/2004

Timothy J. Pelays



INVENTION REPORT

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B&R CODE:

General Procedure

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 (I) Each page of the description, including any drawing(s) or photograph(s), must be signed and dated by each inventor and two witnesses who have

 (I) Each page of the description in old the entire on the interestion Report.

 (2) Send the original and two copies to the intellectual Professories (IPS) (PNNL) or the Intellectual Property Law Department (IPLD) (IDCD).

 (3) If you have questions, release and the cameroniate IP of the Services (IPS) (PNNL) or the Intellectual Property Law Department (IPLD) (IDCD).

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| ABSTRACT | | |
| | ess for sputter deposition of thin films of | alloys of Bi-Tey Sh-Tey and Bi-Sey f |
| thermoelectric energy conversion | . The approach allows deposition of these file | ns on glass and flexible substrates such |
| Kapton. The process was used to | deposit n-type and p-type films that exhibit p | properties nearly as good as measured f |
| bulk materials. | | |
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| RELEVANT KEYWORDS (O | | |
| lelp Thermoelectric films, thin film | s, power sources | |
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DETAILED DESCRIPTION OF THE INVENTION



The best thermoelectric materials for power generation in the 0°C to 100°C temperature range are semiconductors and related alloys based on the bismuth-antimony-telluride-selenium (Bi-Sb-Te-Se) materials system. This disclosure concerns procedures that have been developed which allow the sputter deposition of thin films of these materials that can be utilized to fabricate high voltage, low power thermoelectric (TE) power sources. Films were deposited by RF magnetors sputtering simultaneously from two of three possible sources, namely, targets made of Bi-Te, Sb-Te, and Bi-Se. RF power supplied to each of the targets, substrate temperature and sputtering gas pressure were varied to determine deposition conditions that resulted in films with appropriate properties. Figure 3 describes the variation of material parameters with sputtering conditions. N-type TE material is obtained by supplying RF power of 30 wants or a SbCTe3 target and 20 wants the BiZTe3 target, and with the substrate at the ambient temperature, whereas p-type material was achieved with power levels of 30 wants and 10 wants to the Sb-Te3 and Bi-Te3 targets, respectively. A sputtering gas pressure of 3 millitor was utilized in both cases. A picture of a miniature thin film TE couple tabricated with the disclosed process is shown in Figure 4.

hundreds of TE couples on flexible material such as Kapton



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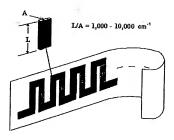


Figure 2. Concept of a TE Module Based on Thin Films on a Flexible Substrate.

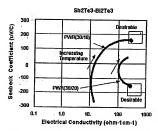


Figure 3. Variation of Seebeck coefficient with electrical conductivity for a range of sputtering parameters.

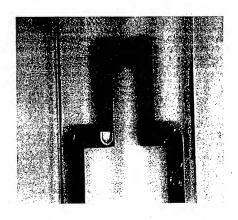


Figure 4. Picture of thin TE couple deposited with the disclosed process.



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From: DeSteese, John G [mailto:john.desteese@pnl.gov]

Sent: Monday, April 14, 2008 3:17 PM

To:

Cc: Matheson, James D; Olsen, Larry C; Silva, Robert R

Subject: FW: Pictures of Test Set-Up

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Lam forwarding Tim Peter's e-mail showing reduction to practice to show the date stamp on the original. John D.

From: Sent:

To: DeSteese, John G

Subject: Pictures of Test Set-Up

Attached





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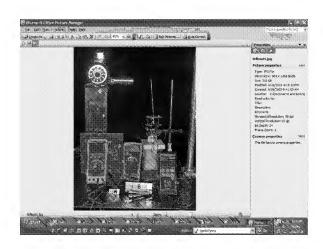
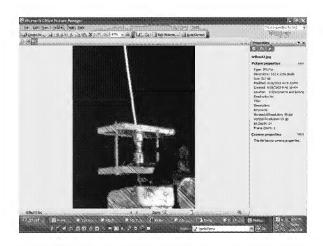




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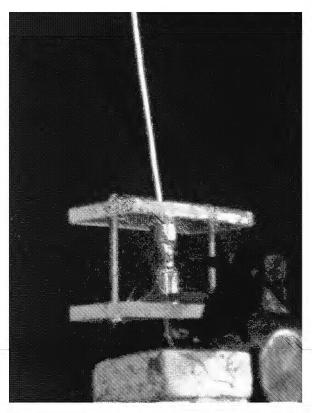
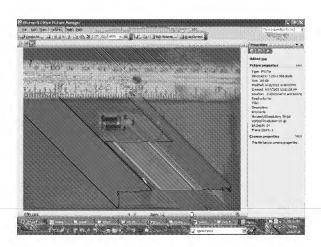


EXHIBIT B-2



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For inventions that may lead to patents, it is a legal requirement that, throughout evaluation and patenting phases, the inventor(s) disclose(s) MATERIAL references (provide copies) that inventor(s) is/are aware of to IP Services.

Examples of MATERIAL information include:

- A. Patents and publications which describe one or more features of the inventions or which would appear similar to the invention. Patents and publications can be our own or others. Publications include reports, conference presentations/proceedings, journal articles, newsletters (Greate), newspaper articles, brochures and flyers;
- B. Information evidencing that the invention, or a closely related invention, was in public use or "on sale" (not necessarily "sold") by anyone more than one year before the filling date of the U.S. application;
- C. Information that the invention, or a closely related invention, was make in the United States by someone other than the inventor named in the patent application; and
- D. Experimental results, either favorable or unfavorable, involving the invention, particularly any comparisons with the prior art. Failure to comply fully with this duty may lead to unenforceability of any resulting patent.

You are NOT required to make a search or to certify that no prior art exists which is more pertinent than that cited. You are only required to answer to the best of your present knowledge.

It is requested that you list in the space provided below those items, if any, of information or date presently known to you that you believe may be MATERIAL to the invention claimed in the above-identified patent application; and that you read carefully the following acknowledgement.

(B) Acknowledgment 1 (we) have read and understood the above description of the legally required duty of disclosurb (we) hereby affirm that to the best of my (our)

| | fy all patents, publications, reports, data, or other documents): | |
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| PUBLICATIONS AND REPORTS: | None | |

ge and halief I (we) have complied with this duty by disclosing to Battelle IP Services as of the date of my (our) signature(s) on the front

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OTHER INFORMATION OR DATE:

(C) General Procedures

Attach a detailed description of the invention to this transmittal sheet; send the originals and 5 copies to Intellectual Property Services (IPS) Department. The detailed description should specifically define what the inventority great as the novel concept and, to the extent possible, how the invention is distinguished from known technology. It should include sketches or photographs that wold help to understand the concept, operative ranges of conditions or constituents, and advantages over similar known concepts. Each page of the description, including any drawing(5) or photograph(5) must be signed and dated by each inventor and two witnesses who have read and understand the invention. If you have questions, please call IP Services 575-2227.

Signatures of Inventors and Witnesses

1 am an INVENTOR and have reviewed the information on the front side of this form, the attached description, and (A) complied with the duty of disclosure statement, (B) filled in the acknowledgment, and (C) followed the general procedures.

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| Signature, Witness I | date Signature, Witness 2 | 10-6-99 date |
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Invention Report on Thermoelectric Device for Ambient Energy Harvesting

October 5, 1999

John G. De Steese

A method for utilizing generally persistent temperature differences that exist naturally between adjacent environments (e.g., earth and the ambient atmosphere) is disclosed as a means of producing electric energy for sensors, monitors and other low-power end uses. This invention appears capable of supplying electric power of up to hundreds of milliwatts perpetually without an external fuel supply or human attention. When combined with rechargeable batteries and power conditioning electronics, this invention could supply a power demand profile that includes brief outputs of tens to hundreds of watts for communications and other higher power requirements.

The concept is illustrated in Figure 1. The core of the device is a series/parallel assembly of miniature thermocouples terminated at a cold and hot shoe at either end of the assembly. The concept can incorporate metallic wire thermocouples and all other thermoelectric materials. Miniature heat pipes are attached to each shoe to improve heat flow to or from the shoes. Power conditioning electronics and a battery may be incorporated and contained in a housing that preferably surrounds the thermocouple assembly.

In operation, one of the heat pipes is inserted into one of the thermal sources/sinks that drive the device. The other end remains in an ambient environment that provides a differential temperature across the thermocouple assembly. For example, the configuration represented in Figure 1 exploits the nearly continuous difference in temperature between earth and ambient air. This difference persists diurnally and seasonally. In summer, the hot shoe would normally be in air and the cold shoe in the ground. In winter, the reverse would tend to occur. In either case, the differential temperature energizes the thermocouples to produce unconditioned electric power of up to hundreds of milliwatts. With appropriate electronic power conditioning, the thermocouples would charge the battery regardless of which end of the device is warmer.

The following example illustrates a representative design. Assuming an average temperature difference between shoes of 20°C and a Seebeck coefficient of 59 µV/°C (e.g., that of a Type E Chromel vs. Constantan thermocouple), an output of approximately 1 mW would be achieved with a series/parallel array of less than 1000 miniature wire thermocouples. It is envisioned that these will be assembled into a robust package using established micro-electromechanical systems (MEMS) technologies. The entire device would be less than 20cm long and 3cm diameter. The heat pipes constitute 70% of the overall estimated length and are amenable to being made shorter for use in some environments (e.g., between hot and cold environments in buildings). MEMS technologies are expected to make construction of larger assemblies (e.g., 100,000 miniature thermocouples) practical. A device with this many thermocouples would raise the unconditioned power of the concept to the hundreds of milliwatts level and higher.

In the potential applications envisioned for this concept, the intrinsically low energy conversion efficiency of thermoelectric elements is not a disadvantage. In comparison to the power demands of typical end uses (e.g., sensors, monitors, locators, etc.) the thermal energy sources of the environments that drive the device are infinitely large. Therefore, energy conversion efficiencies less that 5% are acceptable providing other design requirements (e.g., stored energy density, package size, thermal signature, etc.) are satisfied.

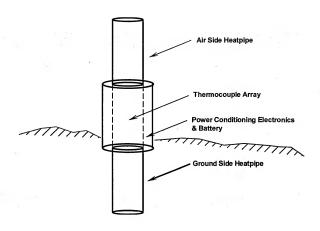


Figure 1: Representative Configuration of Thermoelectric Device for Ambient Energy Harvesting

Inventor Date

Sensors Powered by Ambient Thermal Energy

- Thermal energy scavenged from abundant ambient
- Device is rugged, light weight, suitable for field or facility use
- Perpetual power for life of application
- Independent, maintenance-free electric power for wireless sensing, surveillance, remote actuators and communications
- Potential for miniaturization

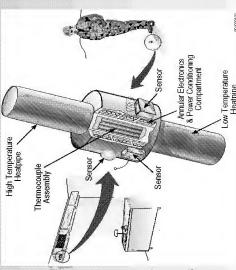


EXHIBIT E - Page 1

Concept Demonstration

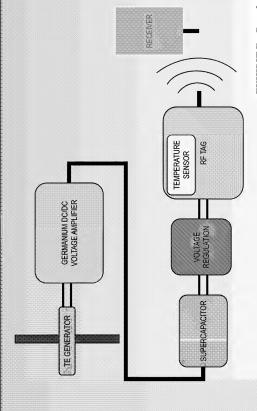
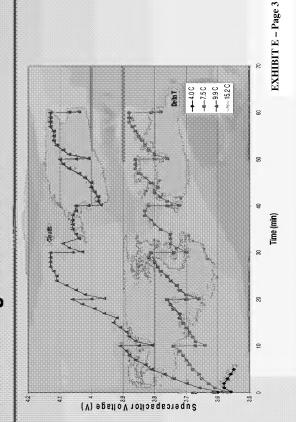


EXHIBIT E - Page 2

Charge Sustainability Demonstration with Solar Heating and Earth Sink



Concept Development

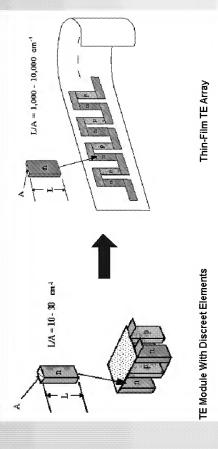
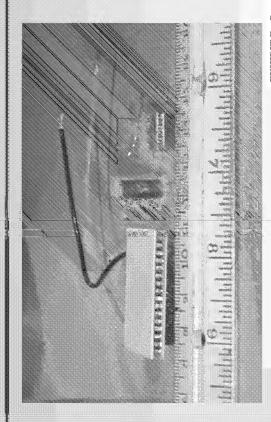


EXHIBIT E - Page 4

Size Comparison Between Thin-Film and Discrete Element TE Generators

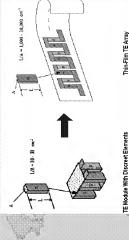


- Summary of Project
- Objective of program is to develop processes for sputter deposition of Bismuth Telluride (Bi-Te) thin films for fabrication of miniature, high voltage thermoelectric (TE) power sources.
- Key results to date: (1) Bi-Te films with good properties deposited on (3) Demonstration TE battery with 24 thermoelements fabricated; glass and 2 mil Kapton;

d Hardina

Technical Approach

- Sputter Deposition Of N- And P-Type Bi-Te Alloys
- Voltage TE Batteries Based On Fabrication of Miniature, High Flexible Substrates (Kapton) Thin Film Thermocouples On

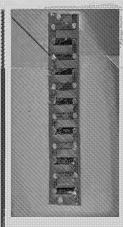


TE Module With Discreet Elements

Milestones

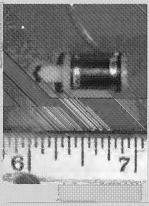
Achieve Sputtered Bi-Te Films With Appropriate Properties Demonstration TE Power Source Based On 2-mil Kapton Prototype Ambient Powered Sensor With TE Battery

- Developed an Approach for Winding Flexible Thin Film Thermocouple Arrays
- Fabricated Demonstration Device to Develop Procedures for Connecting Tapes
- Characterized Demonstration
 Device and Used Results to
 Design 40 TW/1.0 Volt TE Battery

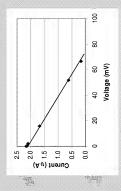


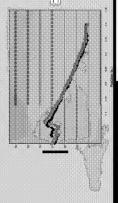
Demonstration Device Utilized Two Flexible TE Strings





- Temperature Distribution
 Determined With IR Camera
- Measurement of Temperature
 Difference Across TE Elements
 Established Performance
 Was As Predicted







Resistance Change vs. Time

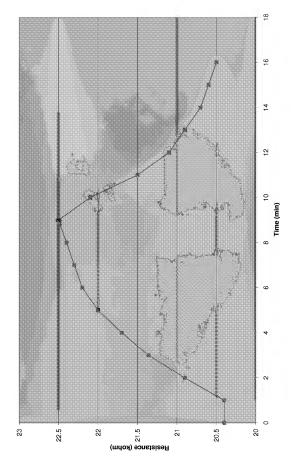
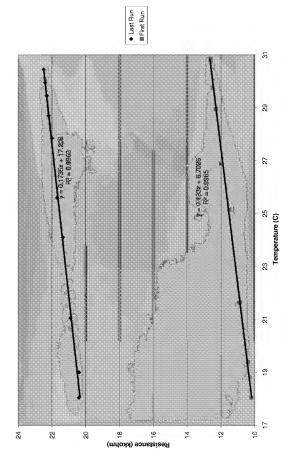
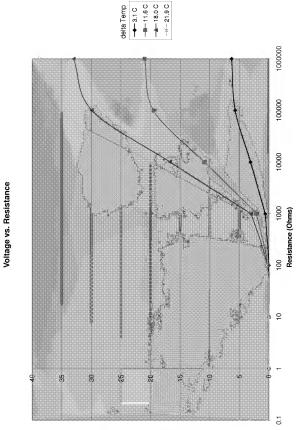


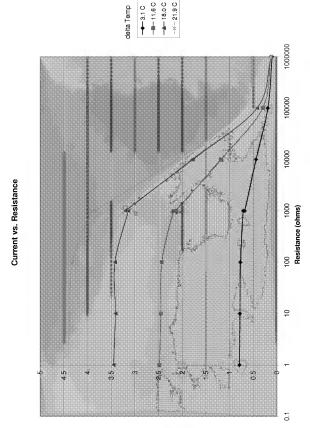
EXHIBIT G - Page 1



Resistance Change vs. Avg.Temp.



Voltage (mv)

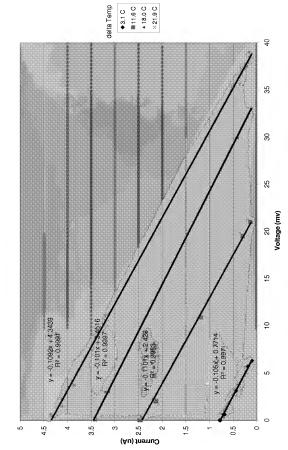


(Au) fuerrent

→#-- 18.0 C

→ 3.1 C

Power to Load (nanowatts)



Current vs. Voltage

Delta Temp (C)

Delta Temp vs. Peak Power

21.9 C → 3.1 C delta Temp 1000000 100000 Resistance (ohms) 88

Power (VI) (nanowatts)

Thin Film Heatpipe - First Lab Bench Tests with gold stripes - 12 junctions

| | Power (VI) | (rieirowatta) | 0 | 1.026 | 9.45 | 9.6 | 29.726 | 12.558 | 3.96 | | | Power (VI) | (nanowatts) | 0 | 0 | 0.486 | 4.578 | 4.28 | 12.862 | 5.85 | 2.73 | | Power (VI) | (nanowatts) |
|---|--|---------------|----------|---------|--------|-------|--------|--------|---------|-------|---|--|--------------------|-----------|----------|---------|--------|--------|--------|--------|---------|--|--------------------|---------------------------------|
| delta Temp = 29.7 C (uncorrected)= 18.0 C (corrected) Too Temp = 46.9 C. Bot Temp = 17.2 C | Power to Load | 0.0119025 | 0.116281 | 1.16964 | 9.8596 | 10.24 | 31.684 | 17.64 | 14.4 | | delta Temp = 19.8 C (uncorrected)=11.6 C (corrected) Top Temp = 36.8 C. Bot Temp = 17.0 C. | Power to Load | (I^2*R)(nanowatts) | 0.0061504 | 0.060025 | 0.59049 | 4.7524 | 4.5796 | 13.924 | တ | 16.9 | delta Temp = 6.6 C (uncorrected) = 3.1 C (corrected) Top Temp = 22.9 C, Bot Temp = 16.3 C | Power to Load | (I'Z'H)(nanowatts) 0.0006241 |
| rrected) | Current F | 3.45 | 3.41 | 3.45 | 3.14 | 3.5 | 1.78 | 0.42 | 0.12 | | rrected) | Current | | 2.48 | 2.45 | 2.43 | 2.18 | 2.14 | 1.18 | 0.3 | 0.13 | rected) = emp = 1 | ent | 0.79 |
| delta Temp = 29.7 C (uncorrected)= 18.0 (on Temp = 17.2 C | Voltage Curre | С | 0 | 0.3 | ო | თ | 16.7 | 29.9 | 33 | | 19.8 C (unco | oltage Cun | (mv) (uA) | 0 | 0 | 0.5 | 2.1 | Ø | 10.9 | 19.5 | 2 | Jelta Temp = 6.6 C (uncorrected) = 3.1 (Fop Temp = 22.9 C, Bot Temp = 16.3 C | oltage Current | (mv) (mw) |
| delta Temp = | Resistance Voltage | • | 10 | 100 | 1000 | 1000 | 10000 | 100000 | 1000000 | | delta Temp = | delta Temp = 19.8 C (uncorrected)=11.6 Top Temp = 36.8 C, Bot Temp = 17.0 C Resistance Voltage Current Power | u) (smyo) | - | 10 | 100 | 1000 | 1000 | 10000 | 100000 | 1000000 | delta Temp = | Resistance Voltage | n) (onms) 1 |
| | g. Temp | 18.05 | 19.4 | 21.65 | 25.15 | 56.9 | 28.95 | 29.75 | 30.8 | 30.85 | | g. Temp | | 19.55 | 20.5 | 22.65 | 25.7 | | | | | | g. Temp | 19.25 |
| | emp Avg | 15.9 | 15.7 | 15.8 | 15.8 | 16.3 | 16.3 | 16.7 | 16.7 | 17.2 | | emp Av | 0 | 16.3 | 16.1 | 16.2 | 16.1 | | | | | | A dme | 16.3 (C) |
| | Temp Bot T | 200 | 23.1 | 27.5 | 34.5 | 37.5 | 41.6 | 42.8 | 44.9 | 44.5 | | Temp Bot T | 0 | 22.8 | 24.9 | 29.1 | 35.3 | | | | | | Temp Bot T | 22.2 |
| | Resistance Top Temp Bot Temp Avg. Temp | 10.2 | 10.4 | 10.9 | 11.5 | 12 | 12.3 | 12.5 | 12.6 | 12.6 | | Resistance Top Temp Bot Temp Avg. Temp | (Kohm) (C) | 20.4 | 20.4 | 2 | 21.5 | | | | | | 90 | (Konm) (C) 20.3 |
| | ш | c | - | Q | ო | 4 | Ŋ | 9 | 7 | ω | | ш. | _ | 0 | - | Q | ო | | | | | | ш | 0 |
| Run 1 | Time | (11111) | | | | | | | | | Run 2 | Time | (min) | | | | | | | | | Run 3 | Time | E) |

EXHIBIT H - Page 1

| 0 0.426 0.408 1.364 1.083 | (nanowarts) (nanowarts) 0 1,728 14,896 14,245 17,78 17,78 17,78 17,7 5,044 17,7 80,28919 |
|--|--|
| | rrected) d F vatts) (Volt. (mv) (Volt. (mv) (Volt. 28983 |
| 0.006084 0.05929 0.5041 0.4624 1.936 3.61 | Incorrected) = 21.9 C (corrected) Current Prome to Load Current Power (VI) (uA) (1°2°F)(Inanowatts) 4.4 0.0194481 0 6.38 0.191844 1.728 3.92 15.3664 14.8265 3.85 14.8225 14.245 5.11 44.521 41.778 0.13 16.9 5.044 Peak Load Cur. (amps) Volt. (mv) Coef(uV/C) 1.396 0.00000044 4.4 118.2796 13.91 1.779E_06 11.78928 84.8373 3.17.779E_06 11.78949 82.42821 44.521 0.000000211 2.1.1 80.28919 |
| 0.78 0.77 0.71 0.68 0.19 0.19 | Jesia Temp = 35.8 C (uncorrected) = 21. [Op Temp = 53.8 C (uncorrected) = 21. [Op Temp = 53.8 C (uncorrected) = 18.0 C John State Jo |
| 0 0.0 0.0 0.0 3.1 5.7 | 75.8 (mv) (mv) (mv) (mv) (mv) (mv) (mv) (mv) |
| 10 1000 1000 10000 100000 1000000 | delta Temp = 35.8 C (uncorrected) = 21.9 C (corrected) Top Temp = 53.6 C (uncorrected) = 21.9 C (corrected) Resistance Voltage Current Power to Load (ohms) (mV) (uA) ("2*R)(nanowatts) 1 0 4.41 0.0194481 10 0 4.38 0.191484 100 0.3 3.8 3.92 15.8624 1000 3.7 3.85 14.8225 100000 3.8 2.11 44.521 1000000 35.4 0.5 25 1000000 35.4 0.13 16.9 1000000 38.8 0.13 16.9 11.6 13.9 1.17804E-06 11.7804 11.6 13.9 1.17804E-06 11.7804 |
| 19.35 | Temp 18.05 19.21.05 22.4.1 22.6.24.1 22.8.7 27.85 28.7 28.4.5 28.4.5 28.7 28.7 28.7 28.7 28.7 28.7 28.7 28.7 |
| 16.1 | Avg. (C) (Avg. 17:5.5. (C) (Avg. 17:5.5. (C) (Avg. 17:5.5. (C) |
| 22.6 | Temp Bot T (5) (5) (6) (7) (7) (8) (8) (8) (8) (8) (8) (8) (8) (8) (8 |
| 20.3 | Resistance Top Temp Bot Temp Avg. Temp (Kohm) (C) 200 (C) 15.5 (B.05 20.4 20.4 15.6 19.5 20.4 20.4 20.4 20.4 20.4 20.4 20.4 20.4 |
| - | |
| | Run 4 Time (min) |